

PRODUCING LIGHTWEIGHT CONCRETE AGGREGATE FROM IRAQI ATTAPULGITE

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This research aimed to produce a type of lightweight concrete aggregate by using available local materials. The lightweight aggregates were produced using methods of sintered strand produced from Iraqi Attapulgit. Clay particle size, firing temperature, and firing soaking time were selected to determine the effectiveness of these parameters on the relative density of produced aggregate. It was found that decreasing particle size has a negative effect, and the optimum firing temperature is 1100°C for 30 minutes. The unit weight density for LWA obtained is about 808 kg/m³, and the relative density is 1.445.

Keywords: Lightweight aggregate, Clay, Relative density, Firing temperature.

1 INTRODUCTION

Structural lightweight concrete (LWC) has many applications in various types of structures (ACI 2003, Chen and Liu 2005). The density of LWC typically ranges between 1440 and 1840 kg/m³ (Neville 2011, Kivrak, et. al. 2006).

1.1 Lightweight Aggregate

Lightweight aggregate (LWA) is a type of aggregate used in the production of lightweight concrete products such as concrete block, structural concrete, and pavement, having low bulk specific gravity (ACI 2003). Most lightweight aggregates (LWAs) are of natural origin, mostly volcanic (pumice, tuff, etc.), and are ready to use, while the remaining types have been developed for factory production from natural raw materials (expanded clay, shale, etc.) by heat treatment. Internal porosity of lightweight aggregate is high, which leads to a low apparent specific gravity (Chi et. al. 2003). High porosity may result in lower strength and low heat conductivity (Campione and Mendola 2004).

1.2 Lightweight Concrete (LWC)

LWC is produced by the following methods: (a) using lightweight aggregate, (b) introducing large voids within the concrete, (c) using coarse aggregate only in the mix (Newman and Choo 2003, Kivrak et. al. 2006).

2 RESEARCH SIGNIFICANCE

Artificial LWA are being produced due to the scarcity of natural sources, manufactured from a widely available material: clay (Arioz et. al. 2008). The main goal of this research is to investigate and produce a new LWC aggregate according to ASTM (2005) from Attapulгите (Palygorskite) clay (Bradley 1940, Liu, et al. 2013, Velde 2010). The formula of the ideal unit cell is $Mg_5Si_8O_{20}(OH)_2(OH_2)_{4.4}4H_2O$, which is available in Iraq in large amounts in the Tar AL-Najaf Injana region, Al-Najaf governorate. Its formation is from the late Miocene–Pliocene as bluish-green and gray clay stone 0.5 m thick.

3 EXPERIMENTAL WORK

3.1 Attapulгите

Table 1 shows the chemical analysis of Attapulгите used.

Table 1. Chemical analysis of Attapulгите after grinding.

Chemical Compound	Oxide content (%)
SiO ₂	51.2
Al ₂ O ₃	8.26
Fe ₂ O ₃	7.90
TiO ₂	0.29
CaO	1.12
MgO	16.4
SO ₃	0.65
Na ₂ O	0.41
K ₂ O	0.38
L.O.I	13.54

Refer to the X-Ray diffraction analysis of Attapulгите, where the presence of Quartz (SiO₂), Palygorskite, Illite, and Calcite (CaCO₃) is in a high percentage, with a low percentage of Hematite (Fe₂O₃) and Feldspar (K₂O.Al₂O₃.6SiO₂). The higher peak of Quartz in the intensity level, and its presence in a high sharpness, is because the Quartz has a high crystalline surface. This causes a high reflection in the X-Ray. The Palygorskite peak has a lower sharpness in intensity level because the surface of clay layer is not crystalline, causing irregular reflection in the X-Ray (Boynton 1980, Lea 1976).

3.2 Production Techniques

Local naturally-occurring LWA of Attapulгите rock in large lumps was used as coarse aggregate. The lumps were manually crushed into smaller sizes by means of a hammer to give a finished product of about 19 mm maximum aggregate size. The aggregate was then screened on a standard sieve series complying with ASTM (2005) as shown in Table 2. The individual size fraction for each batch was recombined in proper proportions to produce the desired grading. The prepared raw material was placed in

loose layers, approximately 100–150 mm thick, on a sinter strand and carried, under drying and ignition hoods fired by gas, in such a manner that baking, initiated at the surface, continued through the full depth of the bed. The gases formed caused expansion; however, in some cases, the cellular structure resulted from the baking of the fuel grains and loss of moisture, and from fusion of the fine particles of the raw material (FIP Manual 1983, European Union 1998, Liu, et al. 2013) as shown in Figure 1. The raw material was reduced to the desired size before firing in a kiln to incipient fusion (temperature of 1000°C to 1100°C), where expansion of the material takes place due to the generation of gases which become entrapped in a viscous pyroplastic mass. This porous structure was retained on cooling so that the apparent specific gravity of the expanded material is much lower than before heating. The temperature can be controlled by using Sager cone. Because a cone measures the heat work rather than the temperature, it is a more accurate indicator of completion of firing than an electric pyrometer (Hamer 2004).



Figure 1. Attapulgite is reduced to the desired size before firing by sager cone.

Table 2. Grading of coarse lightweight aggregate.

Sieve size (mm)	% Passing	% Passing ASTM C330-05
25	100	100
19	95	90-100
12.5	-	-
9.5	30	10-50
4.75	0	0-15

3.3 Determination of the Suitable Firing Temperature for Attapulgite

A laboratory kiln of a maximum temperature 1400°C was used to reach the suitable firing temperature, having a rate of 5°C/min, and when the kiln temperature reached the required degree, the samples were treated for 30, 60, and 90 minutes. Then, the cooling phase of the model started gradually overnight by opening the kiln door very slightly to allow heat exchange with the laboratory temperature. The Attapulgite samples were baked under temperatures ranging between 1000°C-1200°C. When heat was first

applied, the absorbed water was removed and, as the temperature increased, the interlayer and hydrated water removed too from 100°C to 1000°C, as shown in Figures 2 to 6. This represents a steep increase in relative density and a corresponding decline in absorption percentage with the temperature increase.

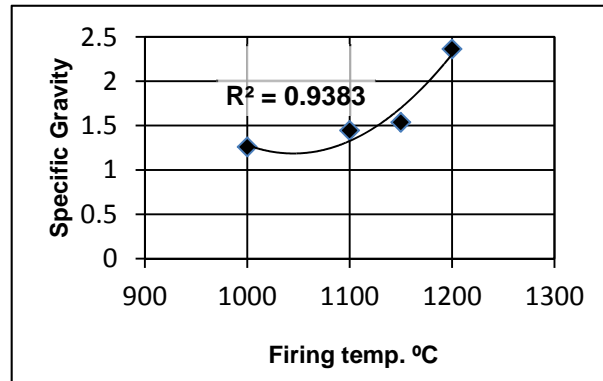


Figure 2. Firing temperature and specific gravity.

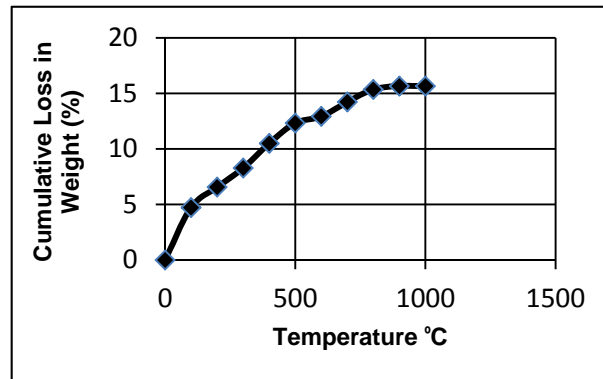


Figure 3. Loss in weight with temperature.

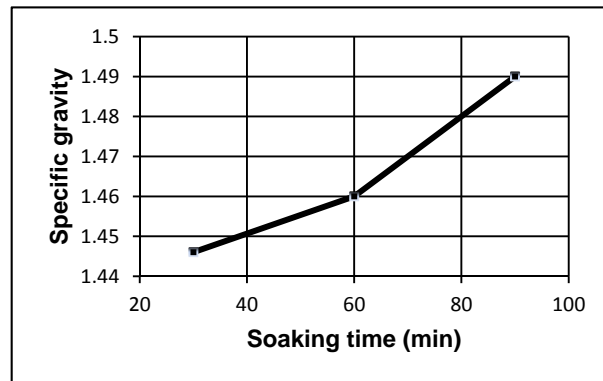


Figure 4. Effect of soaking time temperature on specific gravity at 1100°C.

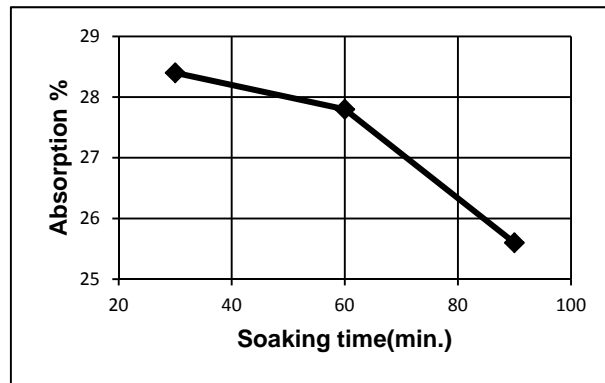


Figure 5. Effect of soaking time temperature on absorption at 1100°C.

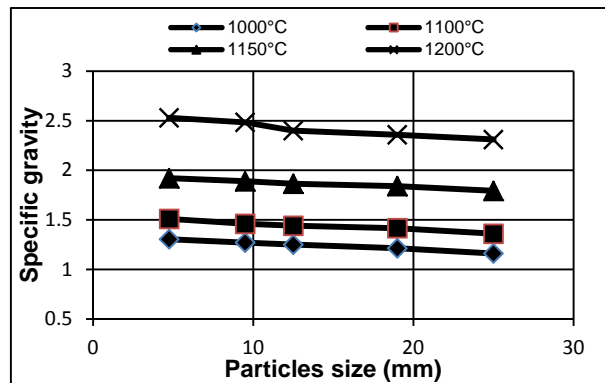


Figure 6. Effect of firing temperature on the specific gravity of different particle sizes.

3.4 Effect of Temperature

Temperature's effect on production was evidenced separately, as shown in Figure 4. It was found that decreasing clay particle size has a negative effect on relative oven dry density.

4 CONCLUSION

LWA can be produced by using methods of sintered strand produced from Iraqi Attapulgit. It was found that decreasing the particle size has a negative effect, and the optimum firing temperature is 1100°C for 30 minutes. The unit weight density for LWA obtained is about 808 kg/m³, and the relative density is 1.445.

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